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Super-Resolution Algorithms for Ultrasonic Nondestructive Evaluation Imaging

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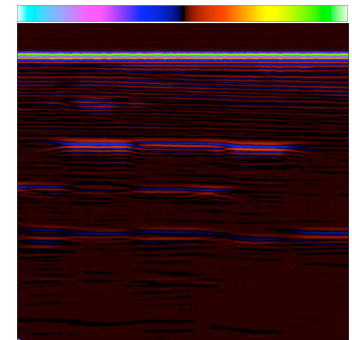
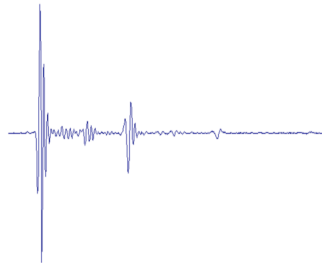


SUPER-RESOLUTION ALGORITHMS FOR ULTRASONIC NONDESTRUCTIVE EVALUATION IMAGING

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JESSIE A. JACKSON

NOVEMBER 29, 2006



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Agenda

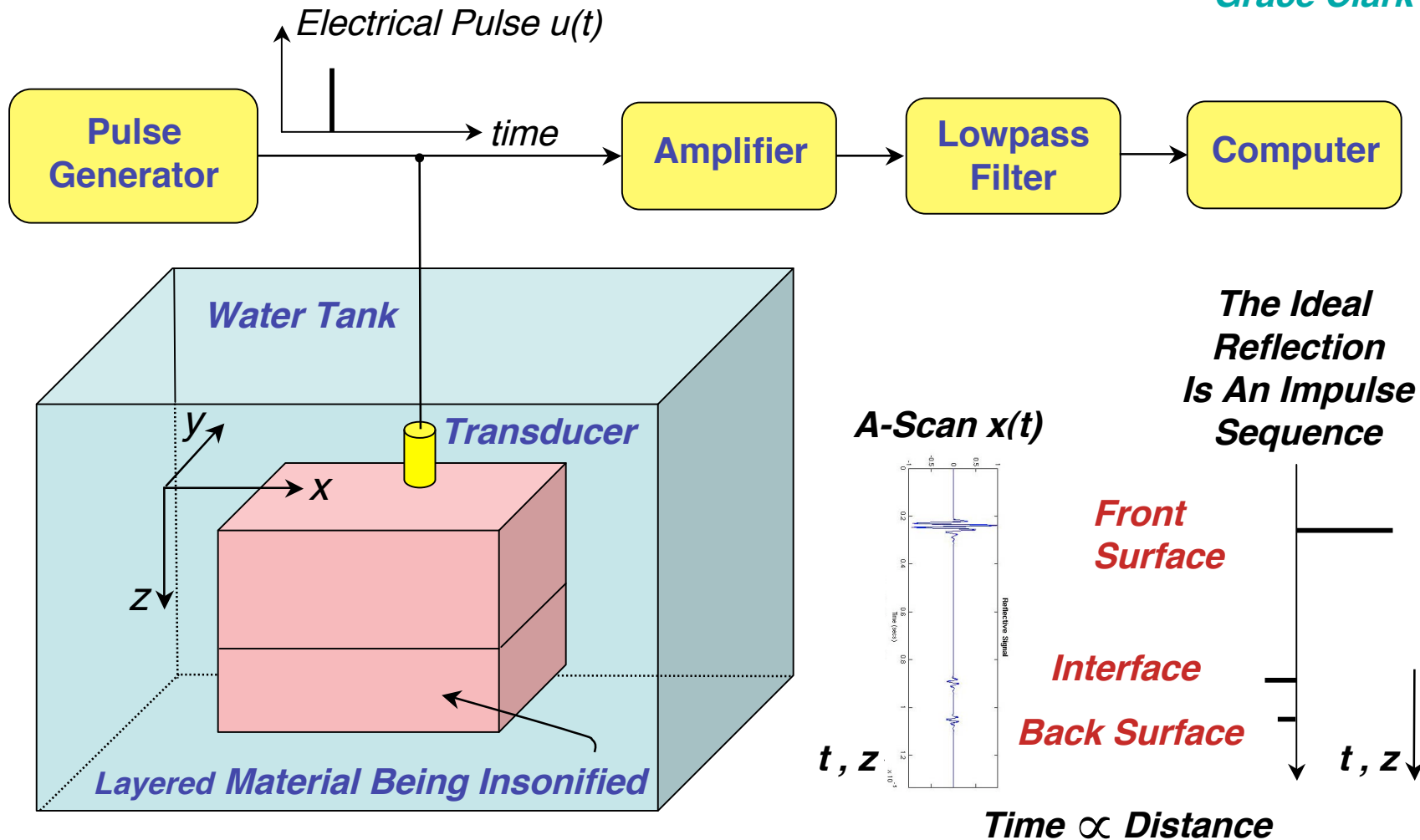


- **Problem Definition:**
 - Ultrasonic NDE measurements
 - The spatial resolution problem
- ***Impulse Response Estimation*** for Enhancing Spatial Resolution
 - Mitigate “ringing” due to the transducer and propagation paths
- ***Bandlimited Spectrum Extrapolation*** for Super-Resolution
- **Examples of Processing Results**

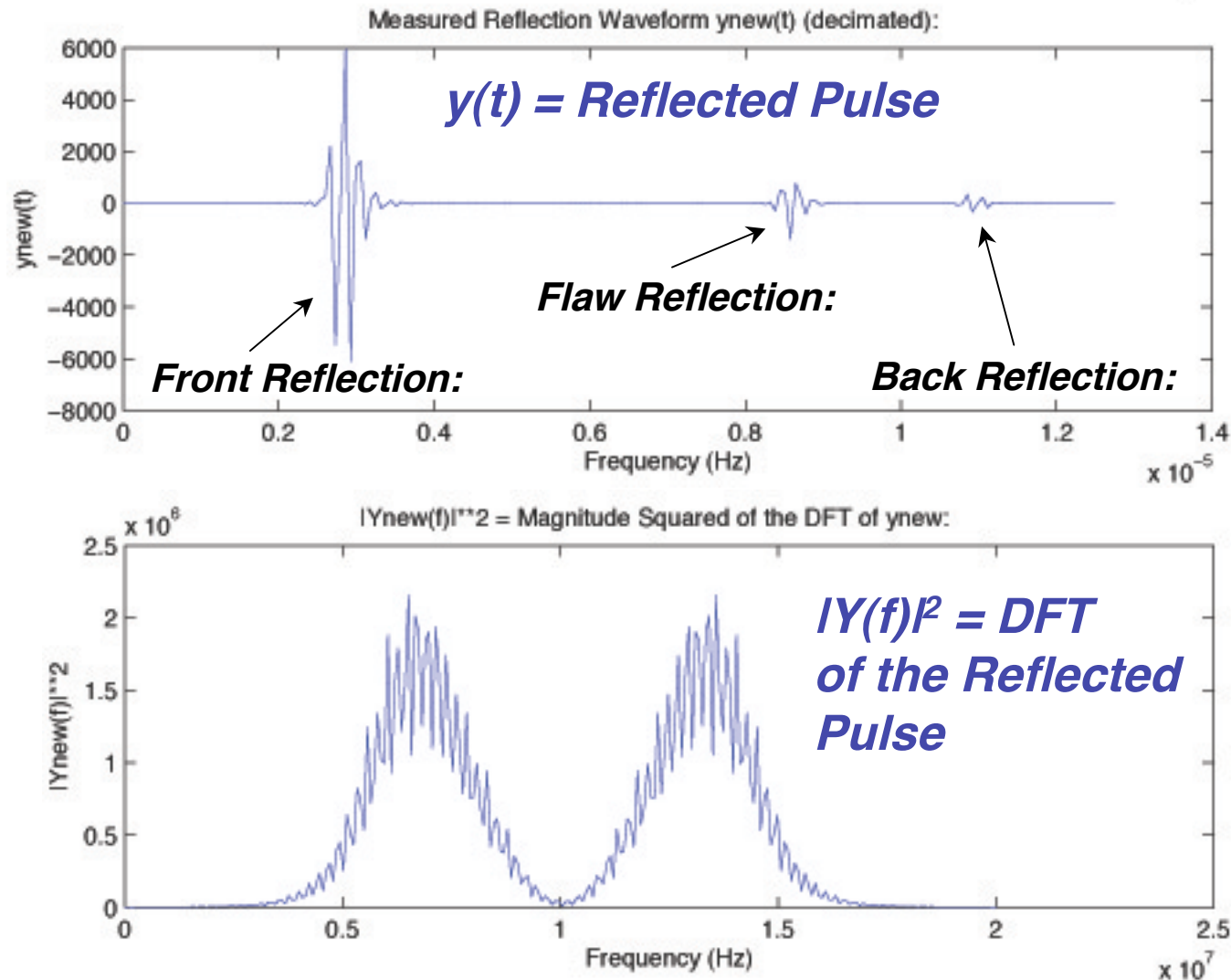
Ultrasonic Pulse-Echo Signals (*A-Scans*) Are *Distorted* By the *Transducer* and the *Propagation Paths* (“*Ringing*”)



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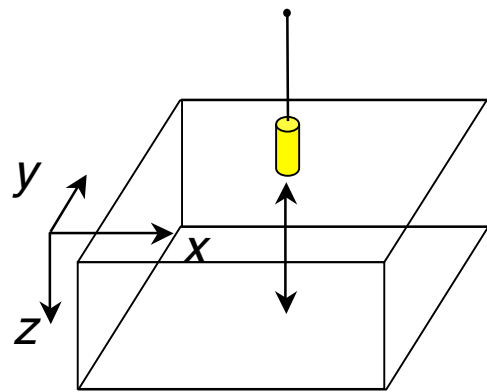


Ultrasonic Pulses Are **Bandlimited** by the Transducer ==> The Pulses **"Ring"**, Reducing Spatial Resolution

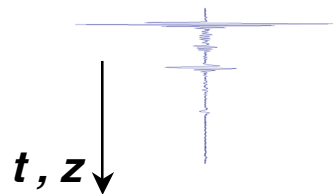


We Define Ultrasonic *A-, B-, and C-Scans* Used in Nondestructive Evaluation (NDE) Studies:

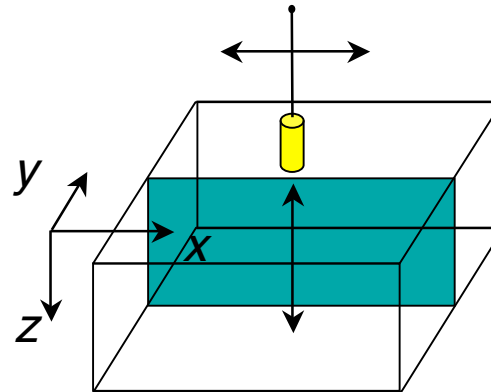
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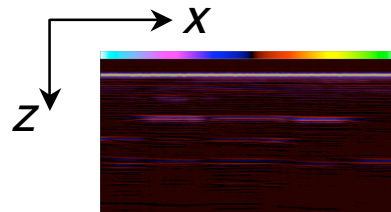
A-Scan $x(t)$
(A Single Waveform)



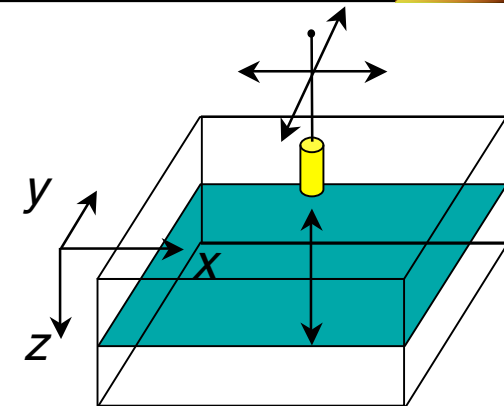
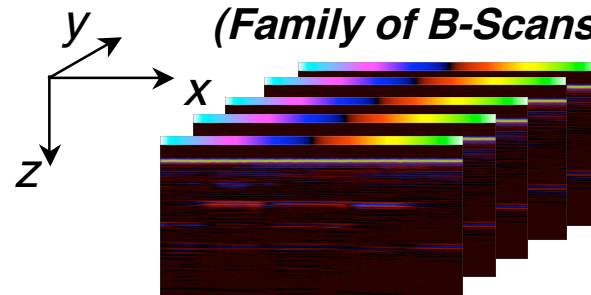
Time \propto Distance



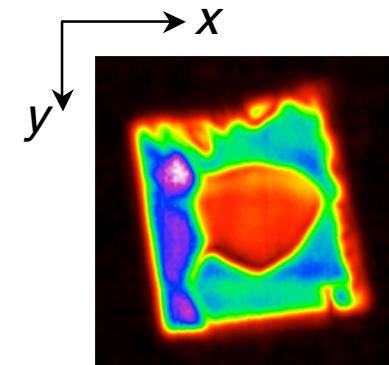
B-Scan
(Family of A-Scans)



3D Volume
(Family of B-Scans)



C-Scan
(Horizontal Slice
At Depth z : Use
A Time Gate)

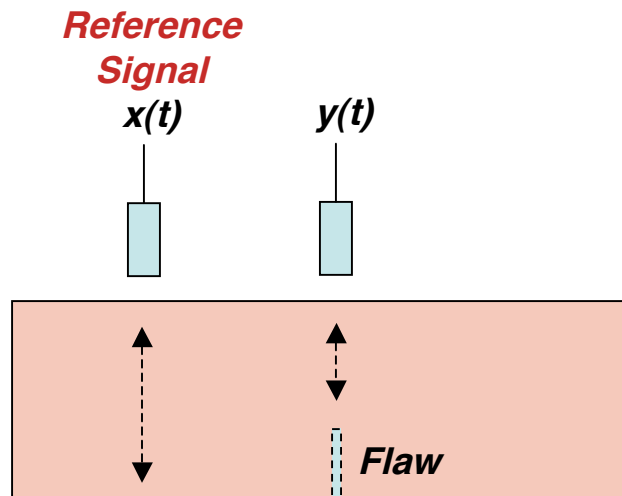


The Reference Scatterer is Chosen to Provide the Transducer / Path Response in the Absence of a Flaw

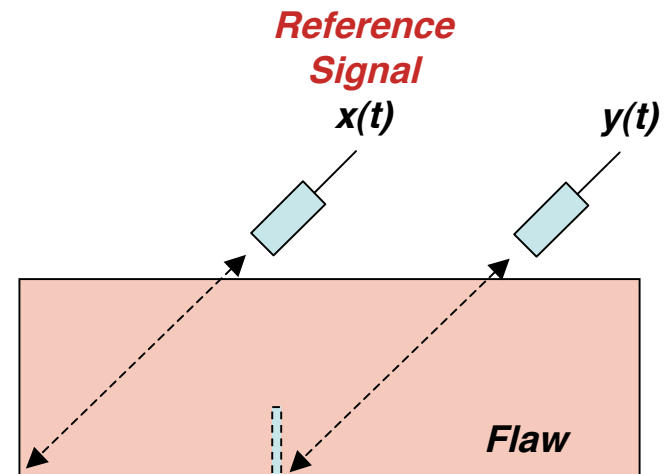


Desired properties of the reference scatterer:

- ***Reflects back most of the energy***
- ***Resembles some feature associated with the flaw environment***



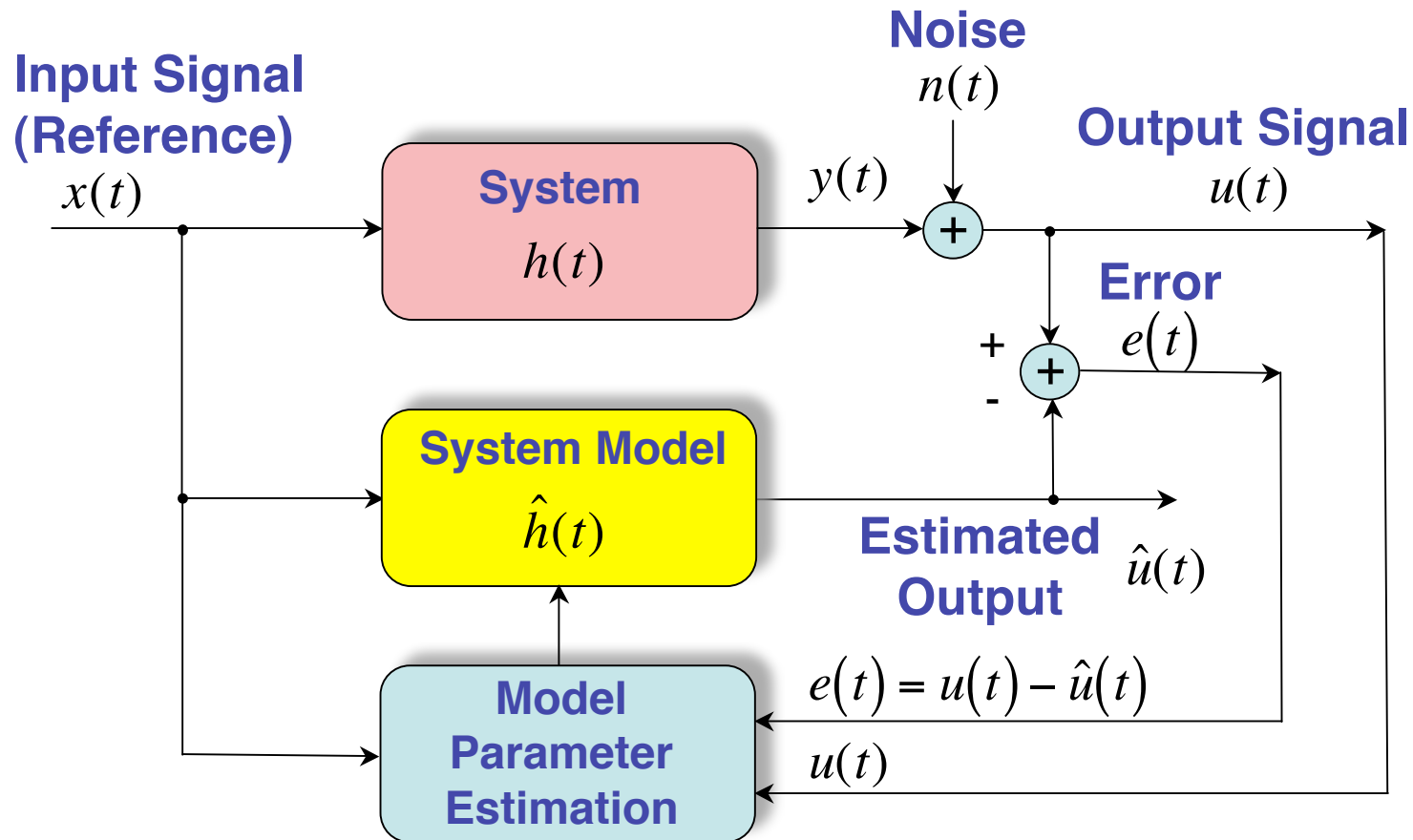
***Front or Back
Surface Reference***



***Corner Reflector
Reference***

System Identification: Estimate the Impulse Response $\hat{h}(t)$

Given: $x(t)$ and $u(t)$ **Estimate:** $\hat{h}(t)$



The Inverse Problem Is Very Difficult

➡ *We Must Regularize the Problem*



- Ill-Posed
(Infinite Number
of possible
solutions)
- Bandlimited
Transducer
Spectral
Response
- Ill-Conditioned -
Numerical Errors
Due to Spectral
Zeros

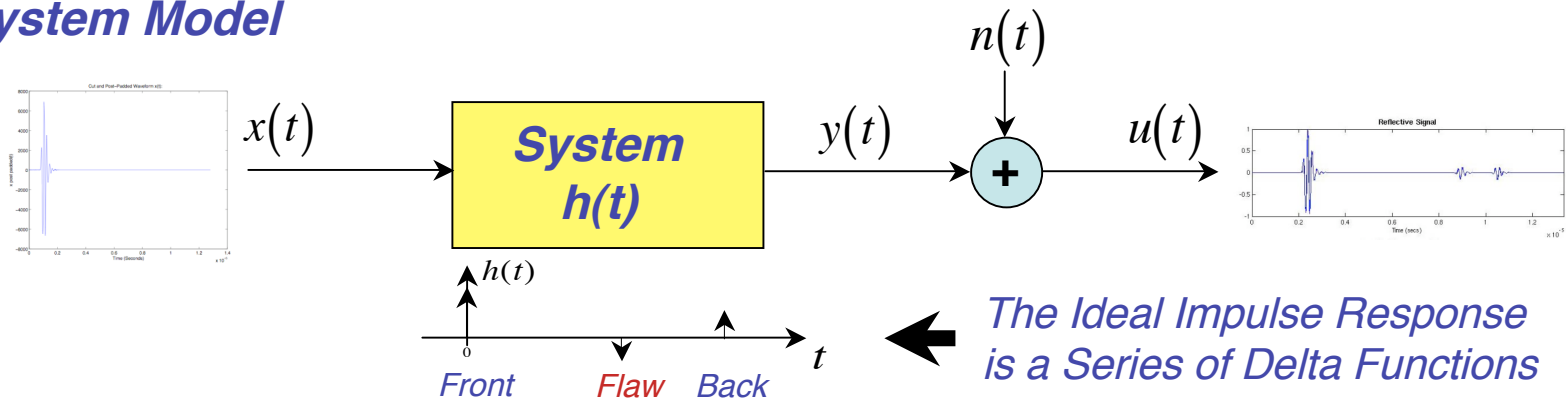


The *System Model* and *Processing Algorithms* Are Summarized in Block Diagrams

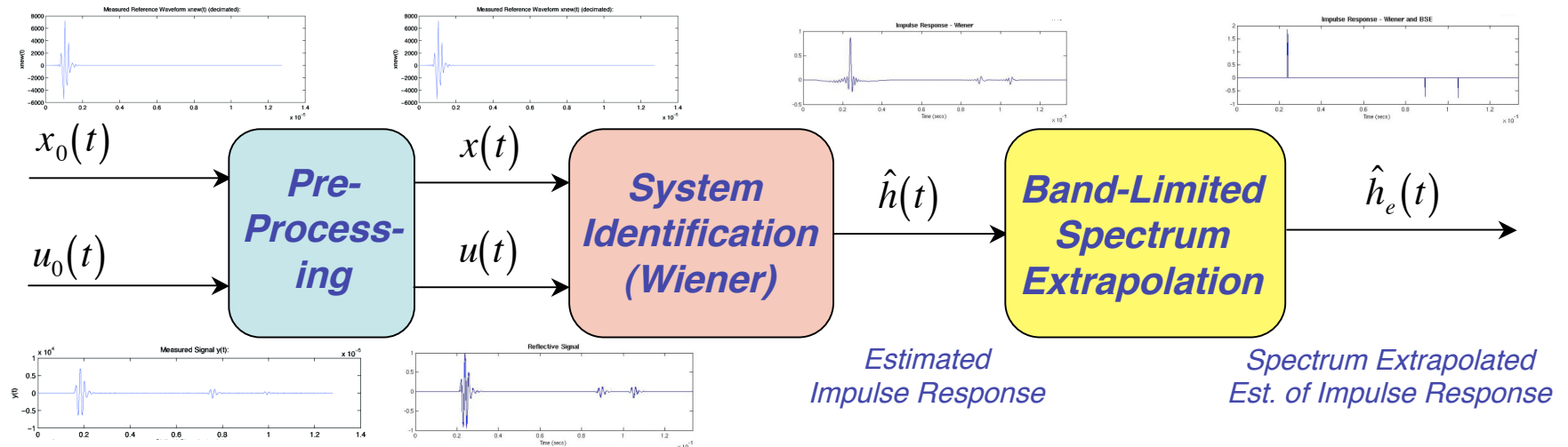
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System Model



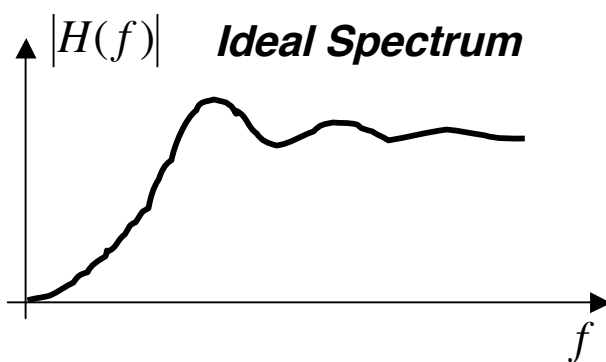
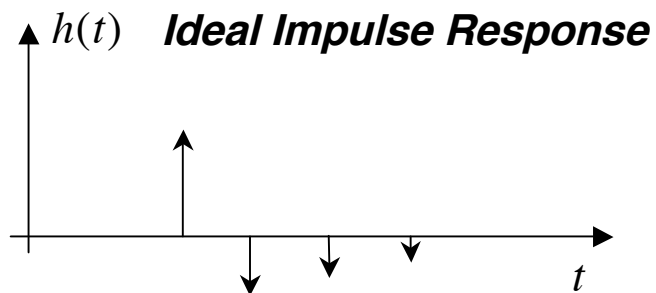
Processing Algorithms



We Use *Bandlimited Spectrum Extrapolation* To Improve *Spatial Resolution*

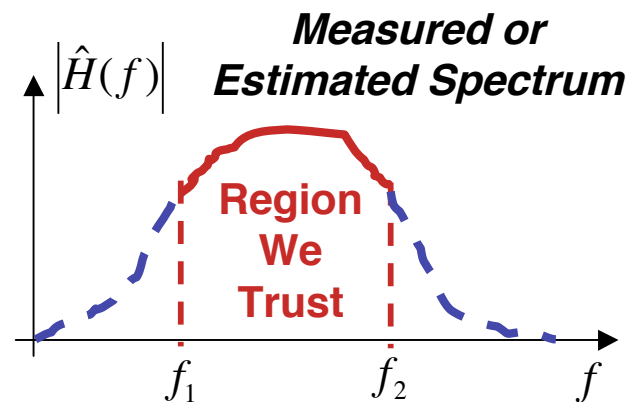
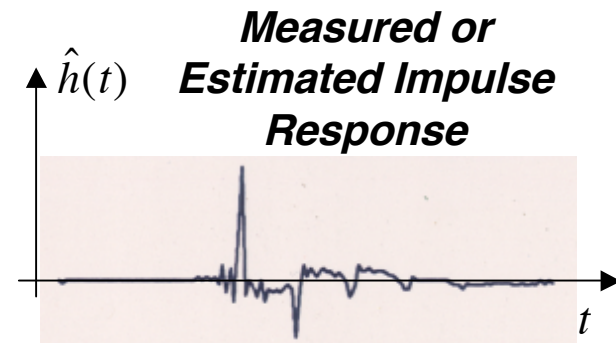


Ideal



$h(t)$

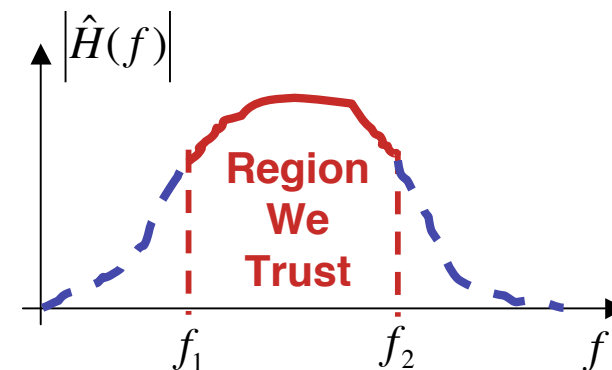
Measured or Estimated



Complex Variable Theory Gives Us a Solid Theoretical Basis for Spectrum Extrapolation



- Our temporal signals have *bounded support*:
 - They are transient (finite length) signals in the time domain
- The Fourier Transform of a signal with bounded support is *ANALYTIC* (continuous, all derivatives exist).
- If any analytic function in the complex plane is known exactly in an arbitrarily small (but finite) region of that plane, then the *entire function* can be found (*uniquely*) by *ANALYTIC CONTINUATION*.



Analytic Continuation Algorithms are Hypersensitive to Noise - *Must Regularize*



- Prior knowledge can be used as constraints to regularize the problem
- Iterative algorithms (*method of successive approximations*) are *slow*, not *unique*, but *can incorporate constraints*.
- Non-iterative algorithms are faster, but can't usually incorporate constraints.
- Often, it is not necessary to determine the inverse of the distortion operator
 - Good for nonlinear or time-varying operators

We Use an Iterative Algorithm for *Regularized* Analytic Continuation

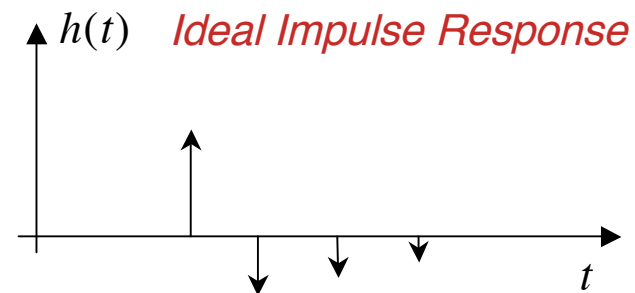


- Estimate the impulse response at the next iteration as a function F of the impulse response at the last iteration:

$$h_{k+1}(t) = Fh_k(t), \quad \text{for } k = 0, 1, 2, \dots$$

- Iterate between the time and frequency domains
(*Method of Alternating Orthogonal Projections*)
- Convergence is proved using contraction mapping theorems from functional analysis
- Use an “*adaptive algorithm*” that assumes the impulse response to be a sequence of impulses - *constrain the time domain signal to be an impulse train*:

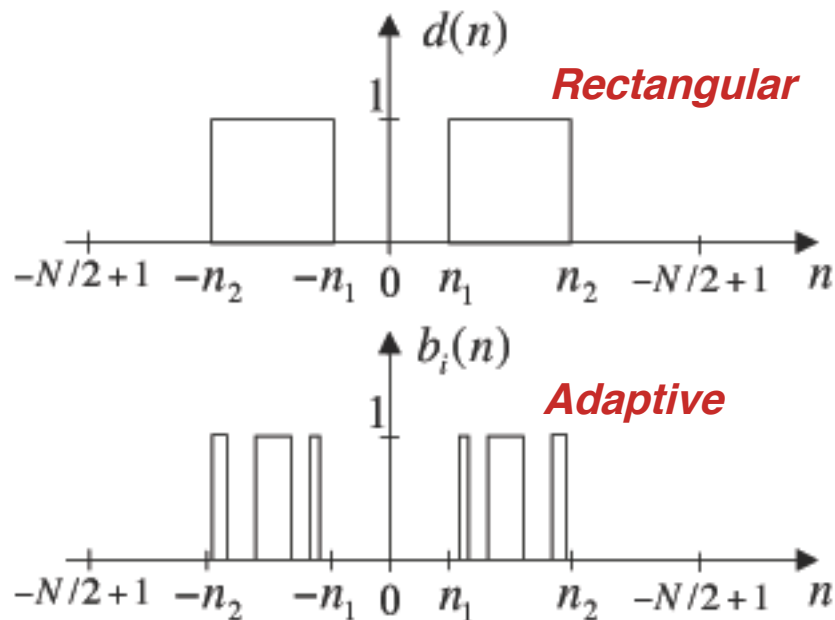
$$h(t) = \sum c_i \delta(t - t_i)$$
$$u(t) = \sum_i c_i x(t - t_i) + n(t)$$



We Constrain the Temporal and Spectral *Support* Using *Projection Operators*

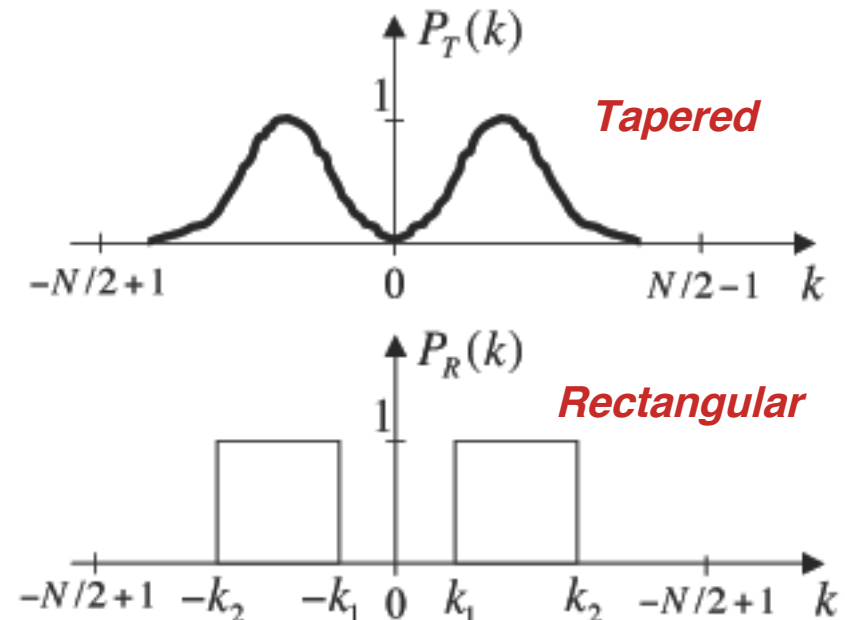


Temporal Projection Operators

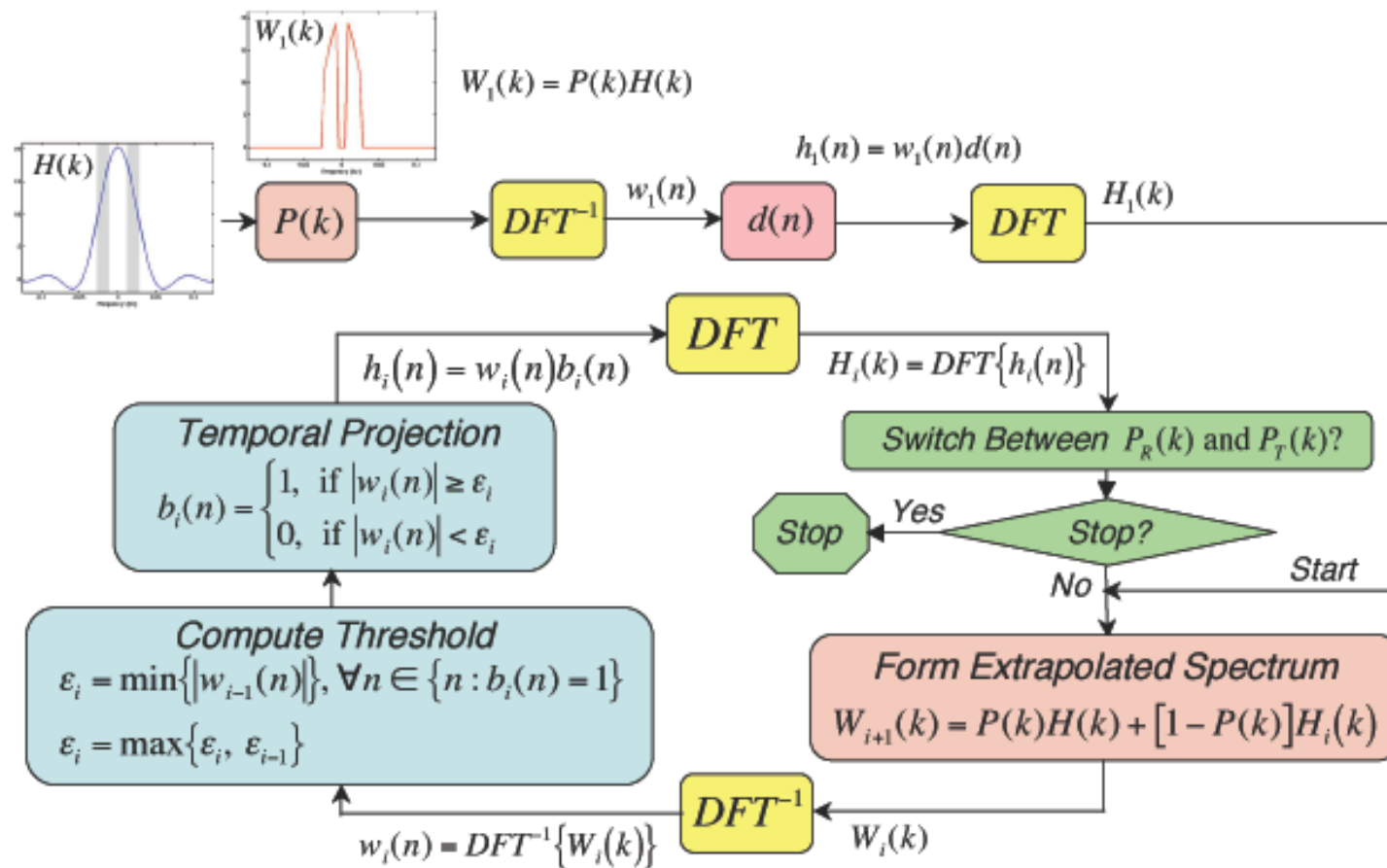


Spectral Projection Operators

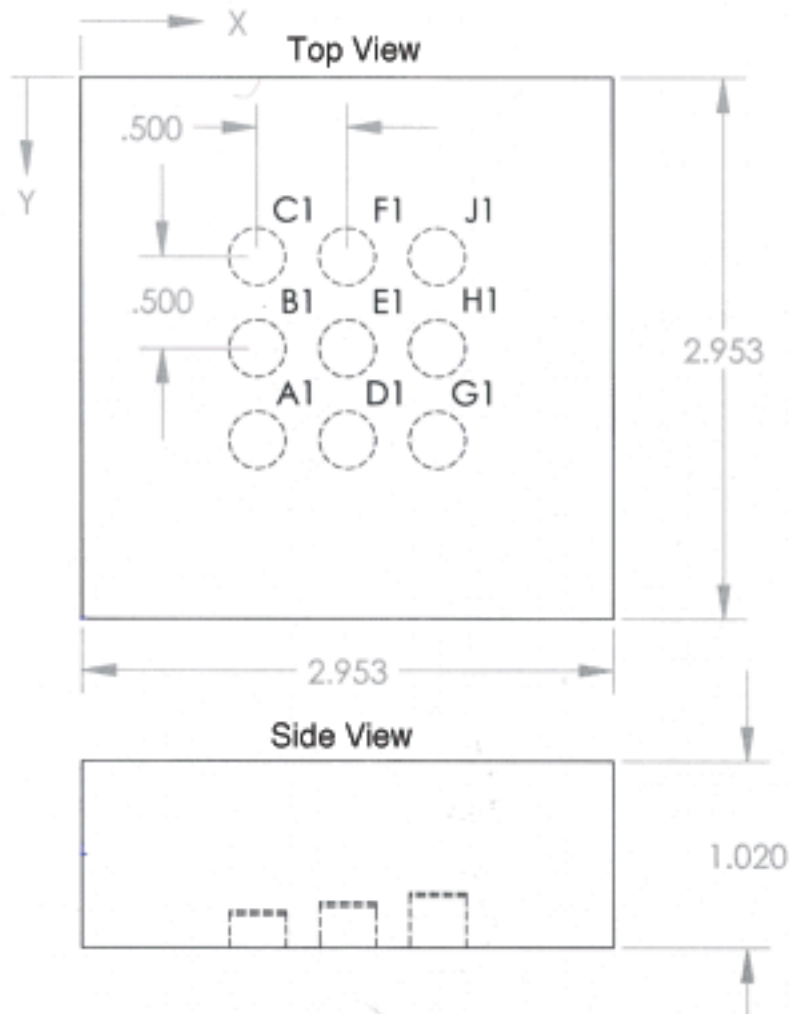
$$P_T(k) = \text{Envelope} \left\{ \frac{|X(k)|}{\max |X(k)|} \right\}$$



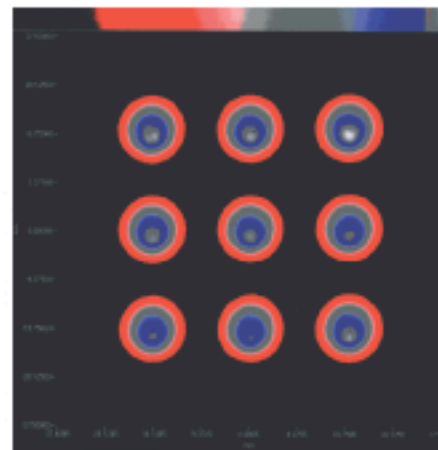
ith Iteration of the Spectrum Extrapolation Algorithm: **Alternating Orthogonal Projections, w/Adaptive Algorithm**



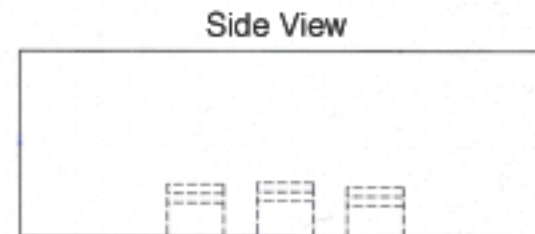
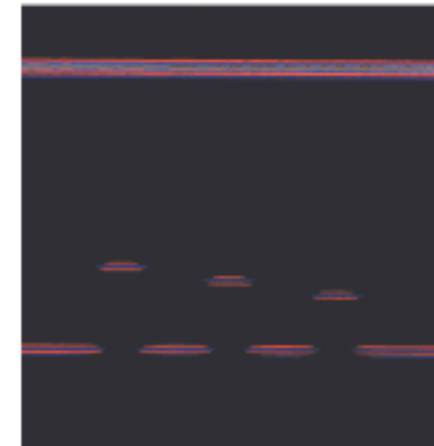
We Constructed a “Phantom” Part - *Aluminum Block* Containing *Flat-Bottom Holes*



C-Scan Image
(Horizontal Slice, Top View)



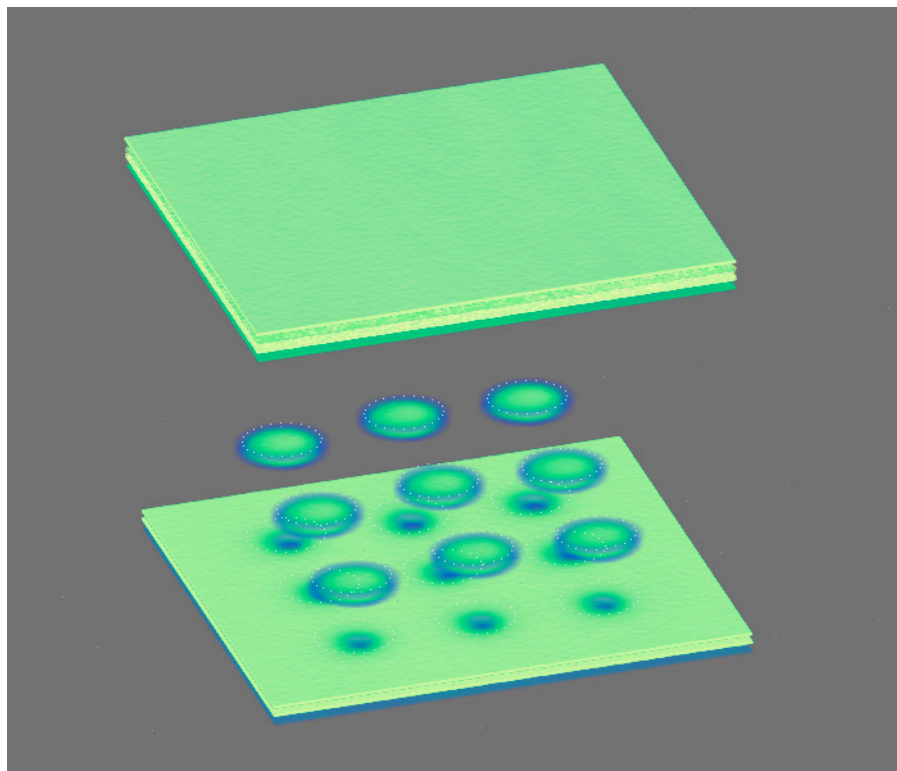
B-Scan Image
(Vertical Slice, Side View)



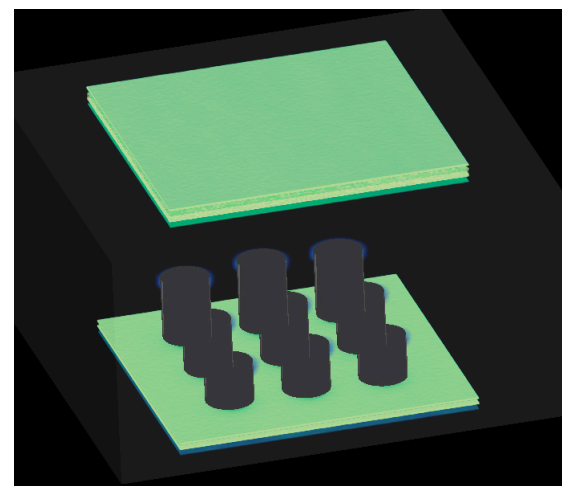
We Can Combine CAD Models With 3-D Data To Clarify Ultrasonic Evaluation Results



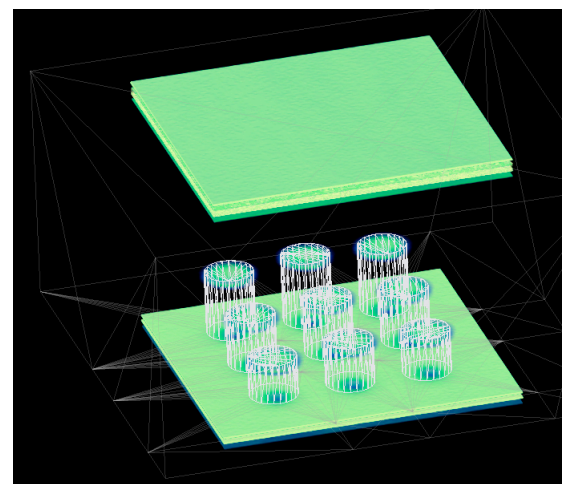
3-D Ultrasonic Data Set



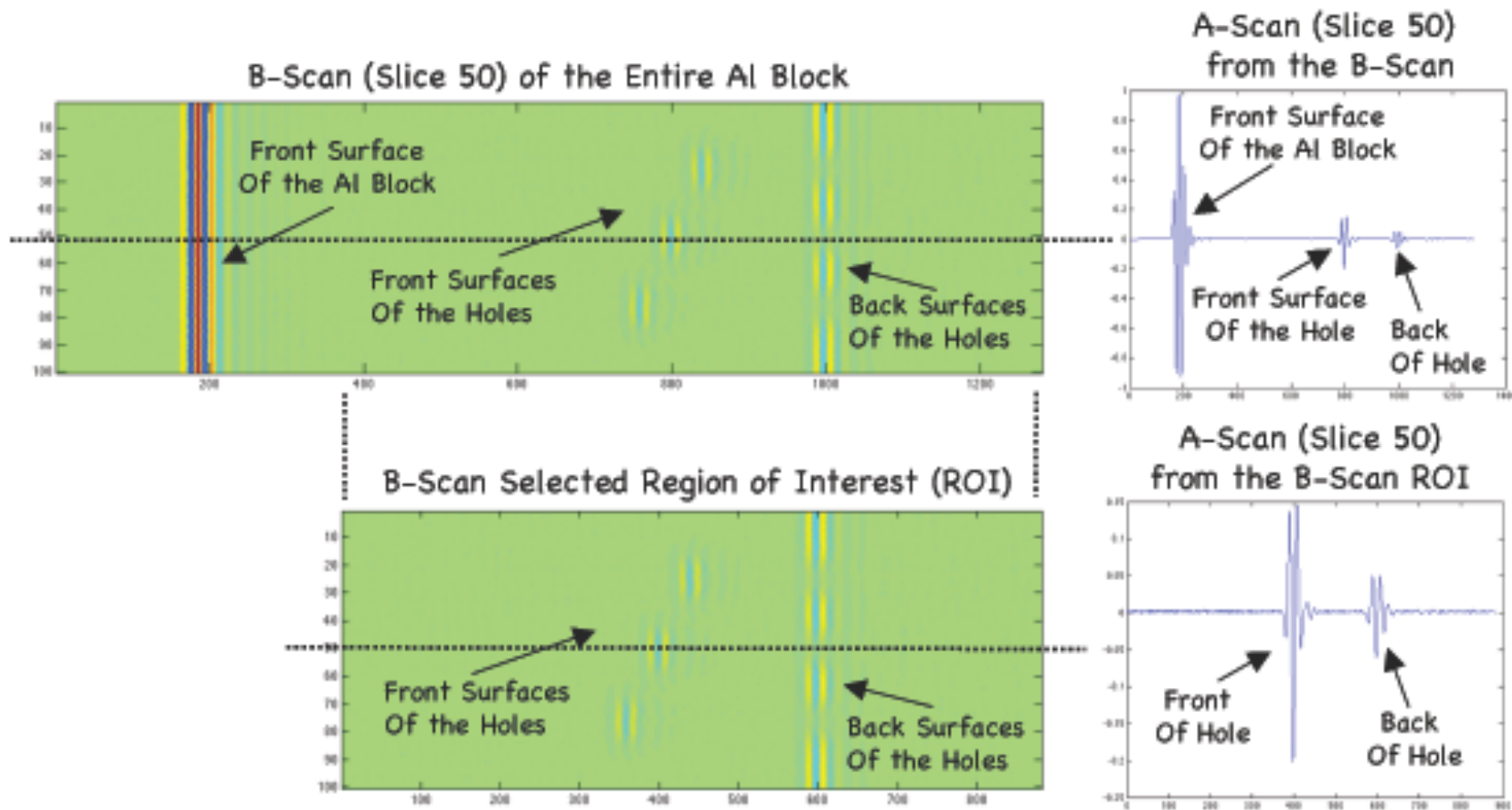
3-D data and **CAD Model-Solid**



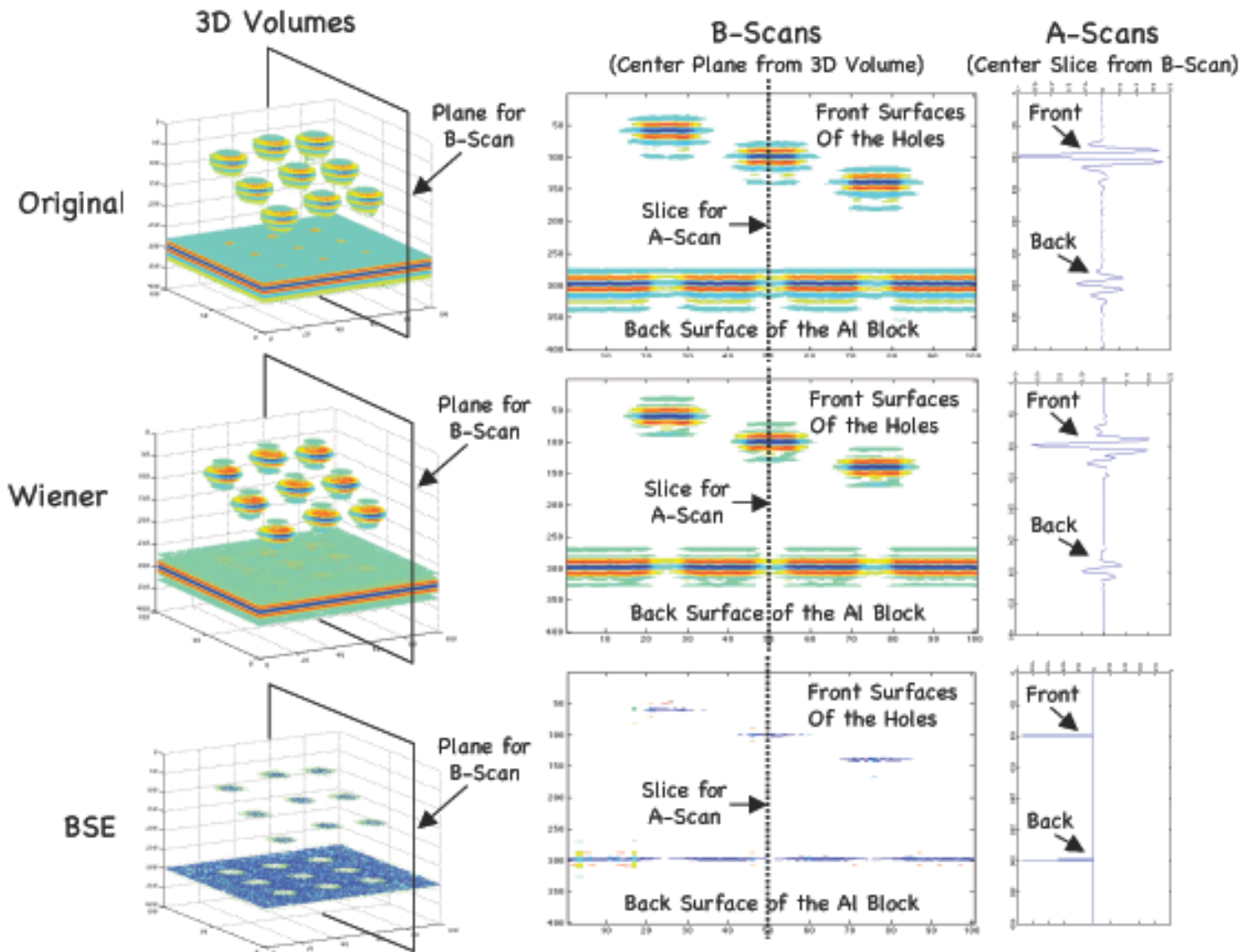
3-D data and **CAD Model-Lines**



A-scan and B-scan Data Show that Material Interface Reflections Are Blurred Because of Transducer Ringing



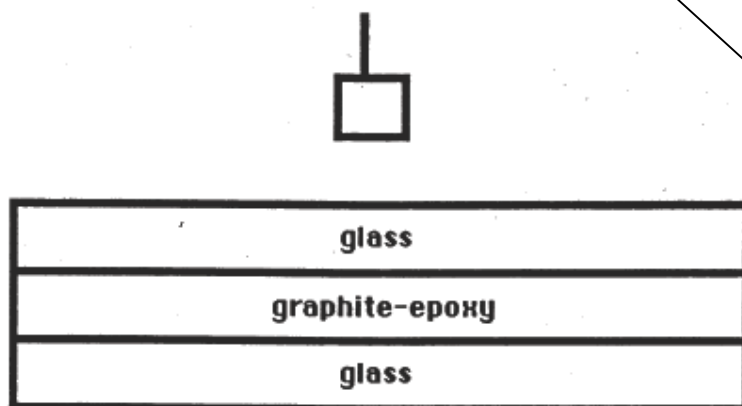
System Identification and Spectrum Extrapolation Results Are Summarized for the *Flat-Bottom Hole Phantom* Signals



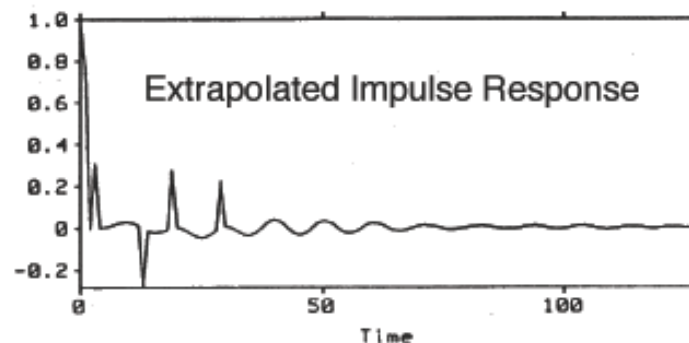
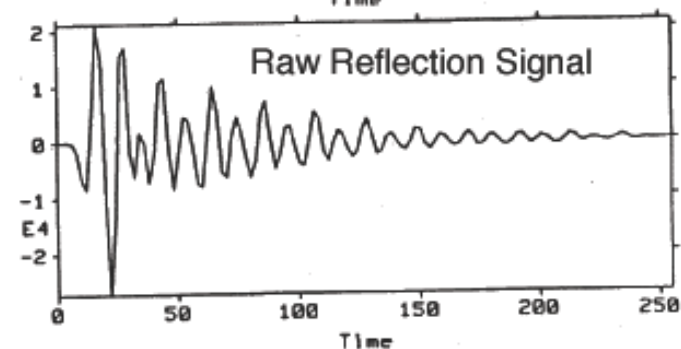
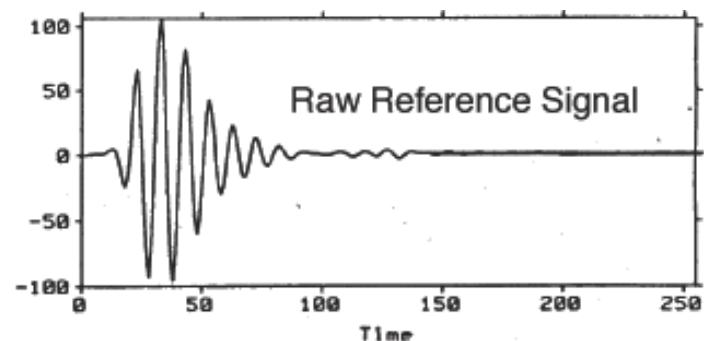
Graphite Fiber Composite Material: *Thickness Measurements from Superimposed Layer Reflections*



The layer thicknesses are much smaller than the transducer ring-down time

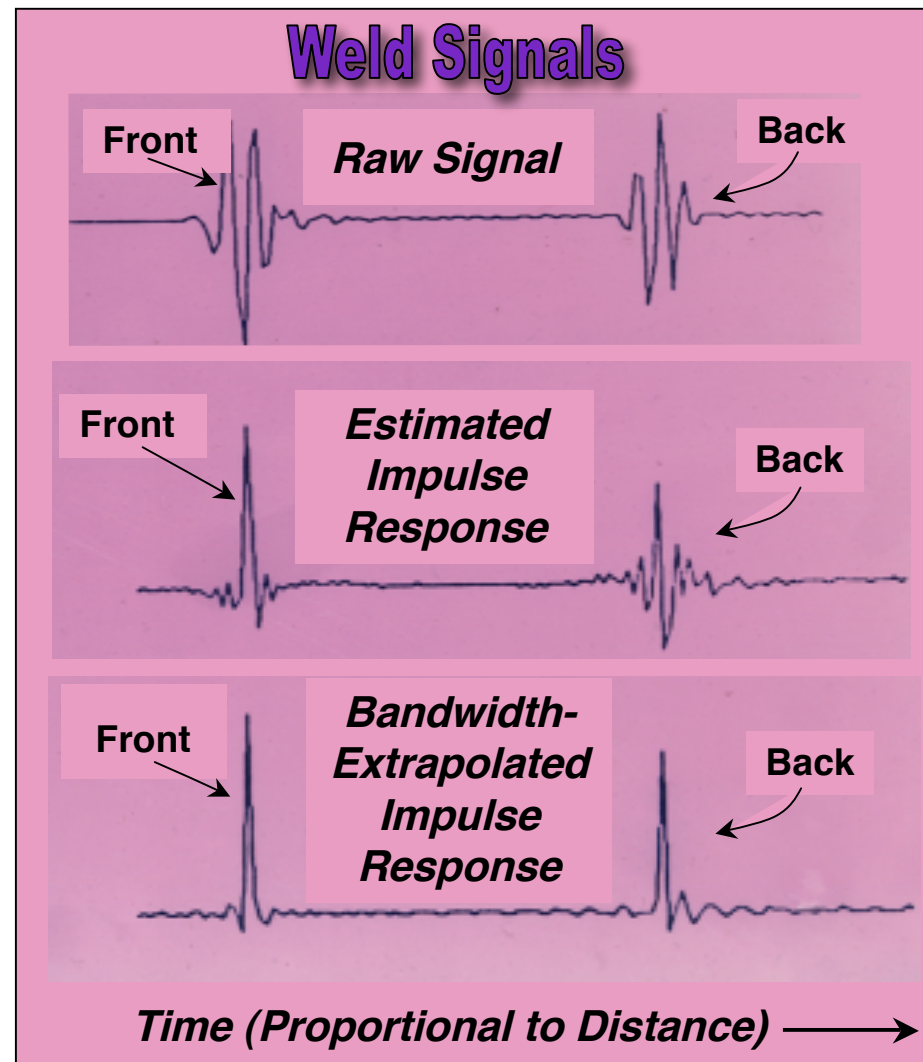
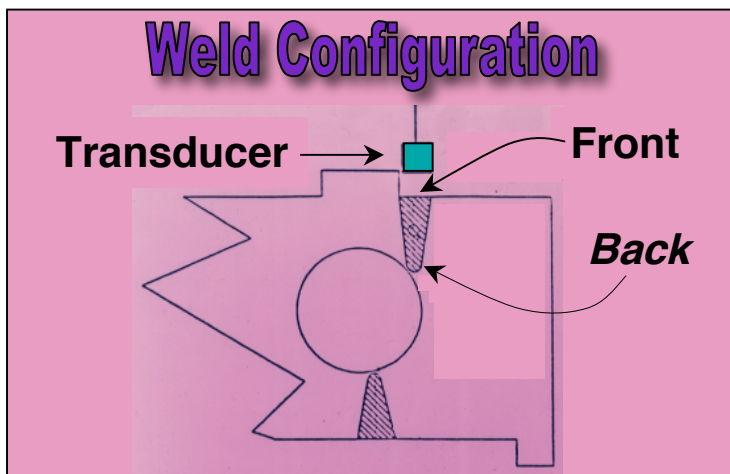
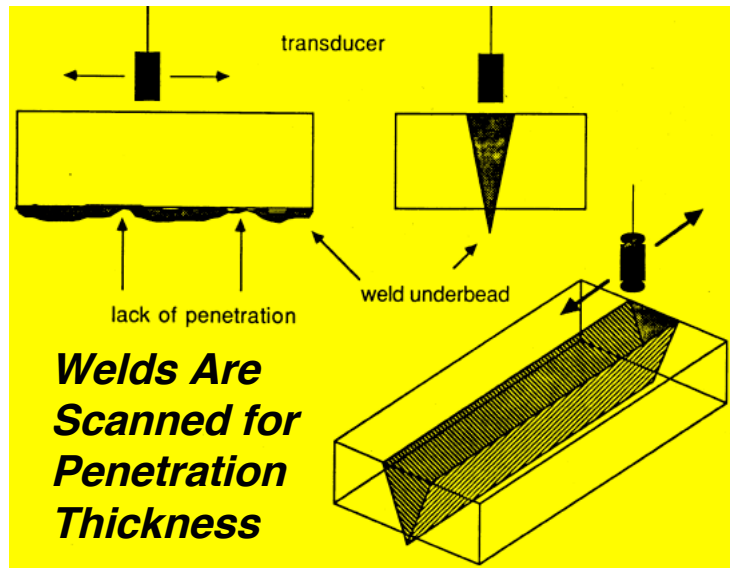


graphite weave
in epoxy

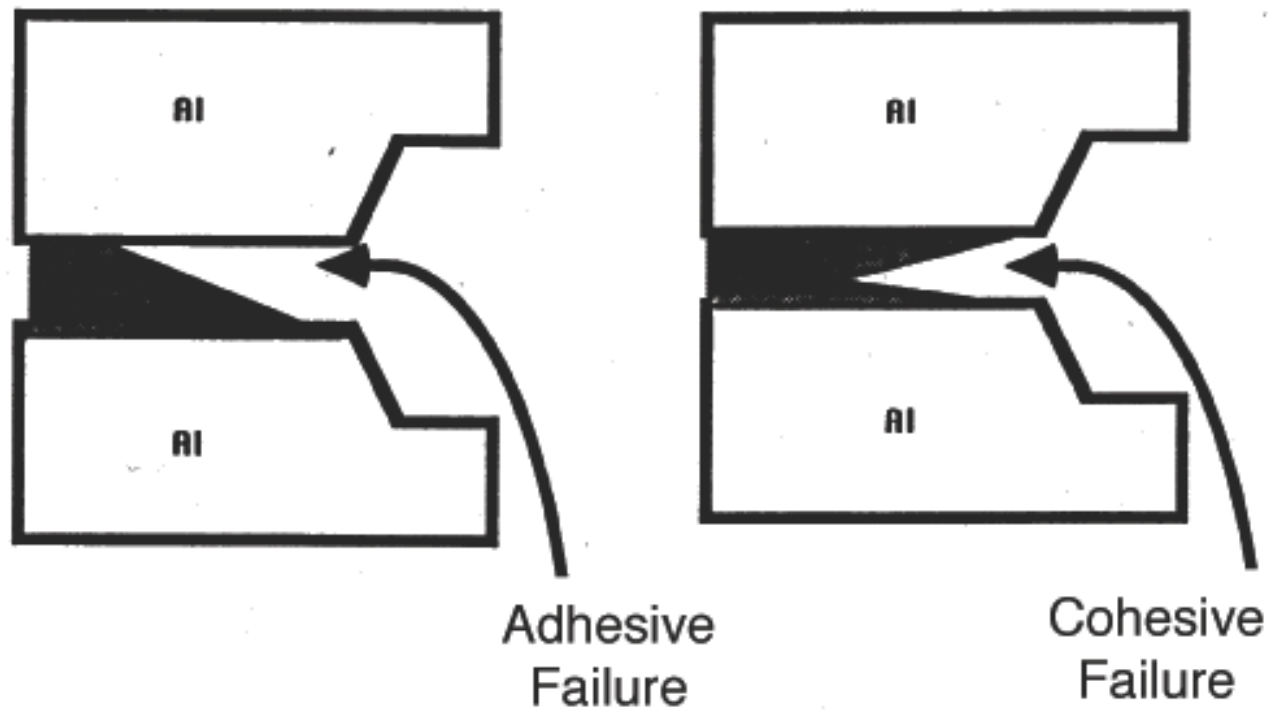


Ultrasonic Pulse-Echo Signals Are Distorted by the Transducer and the Propagation Paths

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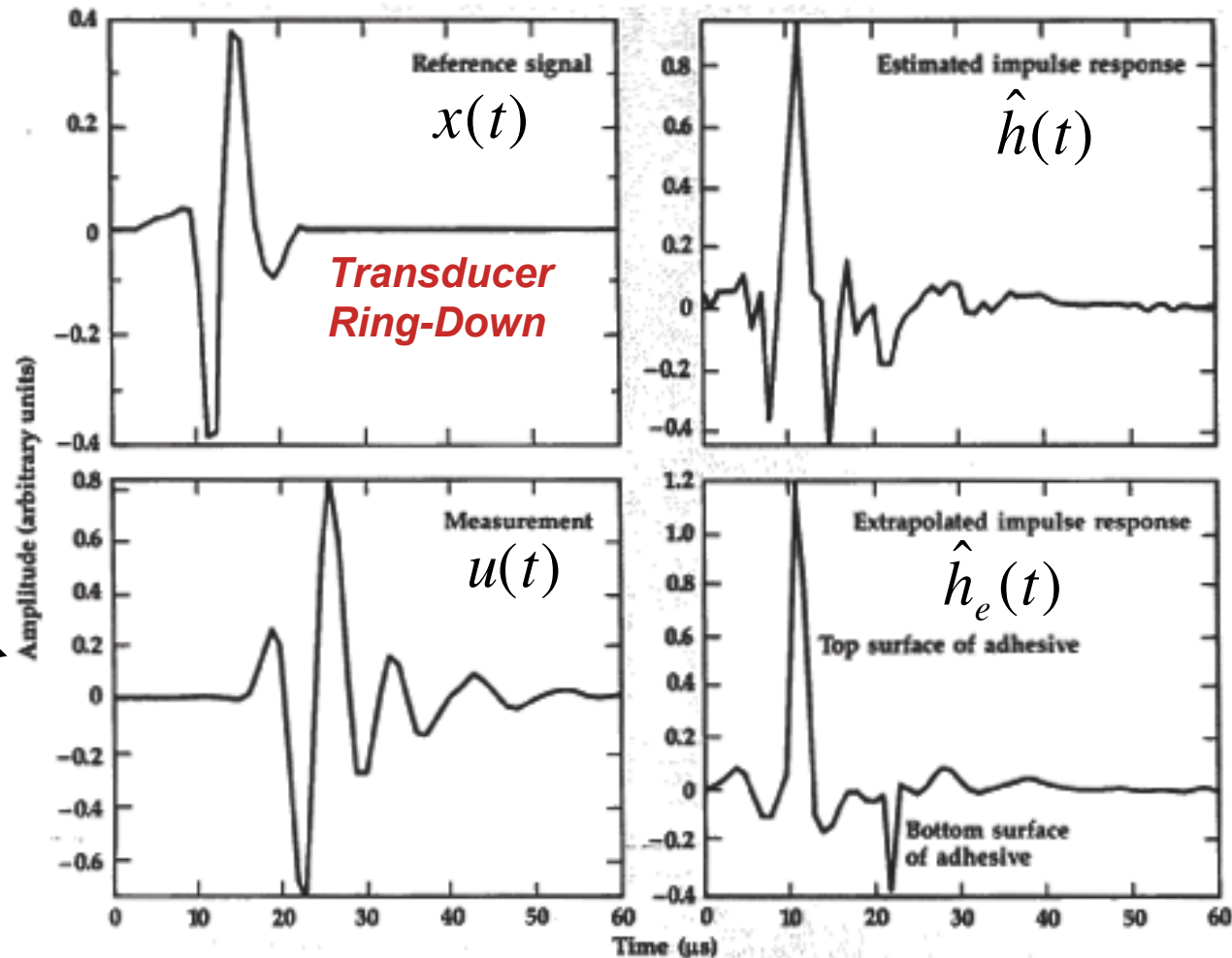
Adhesive Thickness Measurements Require Resolved Layer Reflections



Adhesive Thickness Measurements from Superimposed Layer Reflections



The layer thickness \ll Transducer ring-down time



Conclusions



- We used MATLAB, including a GUI
- The key to dealing with the ill-posed problem is to use:
 - Prior knowledge, when available
 - Proper regularization schemes
- The regularized algorithms provide useful solutions for both simulated and real data sets
- Future work: New programmatic applications

Contingency VG's



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Our Objective is to Improve Temporal Resolution by *Extrapolating Spectra*

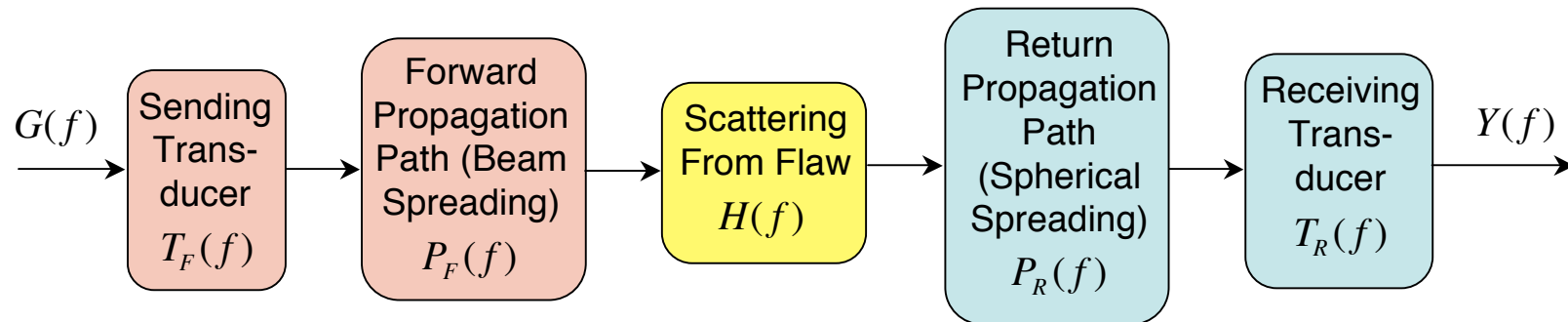


- The transducer bandlimits our signals
 - System identification solutions are not unique
 - System identification solutions are valid only in a finite frequency interval $[f_1, f_2]$.
They give us the optimal least squares solution, given the bandwidth of the transducer.
 - We can never obtain narrow impulses in the time domain
- We wish to extrapolate spectra beyond $[f_1, f_2]$.
 - This can allow us to obtain better approximations to impulses in the time domain.
- We propose to extrapolate the spectra of:
 - $u(t)$ *The measured pulse-echo signal*
 - $\hat{h}(t)$ *The estimated impulse response*

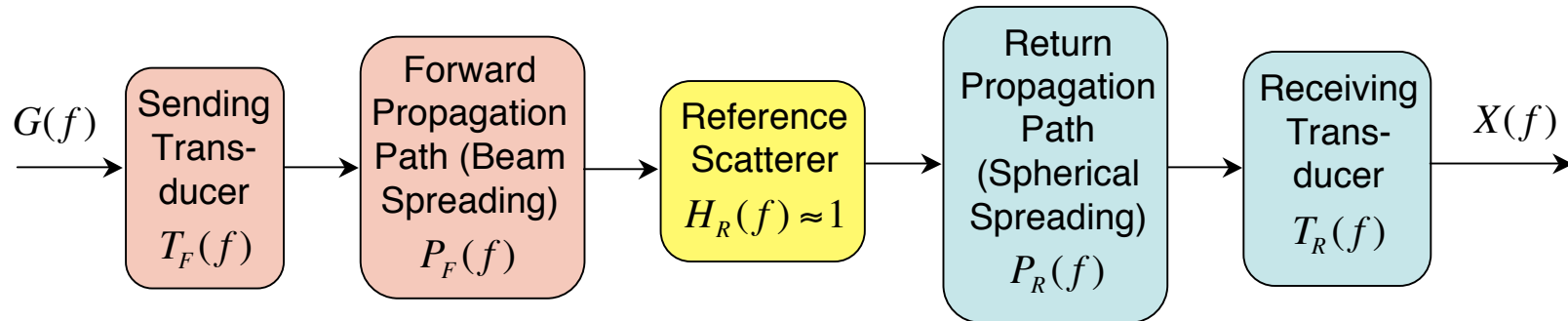
We Use a Reference Scatterer to Help Remove Distortion: Conceptually, This is a “*System Identification*” Problem



Experiment to Measure the Scattered Signal $Y(f)$



Experiment to Measure the Reference Signal $X(f)$



Conceptually:

$$\frac{Y(f)}{X(f)} = \frac{\cancel{T_F(f)} \cancel{P_F(f)} H(f) \cancel{P_R(f)} \cancel{T_R(f)}}{\cancel{T_F(f)} \cancel{P_F(f)} (1) \cancel{P_R(f)} \cancel{T_R(f)}} \approx H(f) \xleftrightarrow{F^{-1}} h(t)$$